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Perspective

Perspective on hetero-deformation induced (HDI) hardening and back stress

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ABSTRACT

Heterostructured materials have been reported as a new class of materials with superior mechanical properties, which was attributed to the development of back stress. T … nts with no consens … ress, making t … ard domains appear w … d from interacti … scribed as hetero … ’ should be rena …

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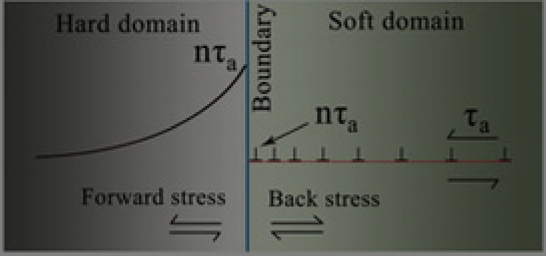

IMPACT STATEMENT

The ‘back stress’ hardening in the literature can be described more accurately as hetero-deformation induced (HDI) hardening and the measured ‘back stress’ should be renamed HDI stress.

KEYWORDS: Heterostructured materials strain gradient back-stress forward stress hetero-deformation induced (HDI) hardening

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Background

Heterostructured (HS) materials have recently attracted extensive attention from the materials community, as evidenced by the increasing number of international conferences and publications in recent years. For example, a symposium entitled ‘Heterogeneous and Gradient Materials III’ was held in the TMS Annual meeting in March 2019. A Gordon Research Conference on Heterostructured Materials will be held in June 2019. A symposium on Nanostructured, Heterostructured & Gradient Materials will be held in the Chinese Materials Conference in July 2019. Figure 1 shows that the number

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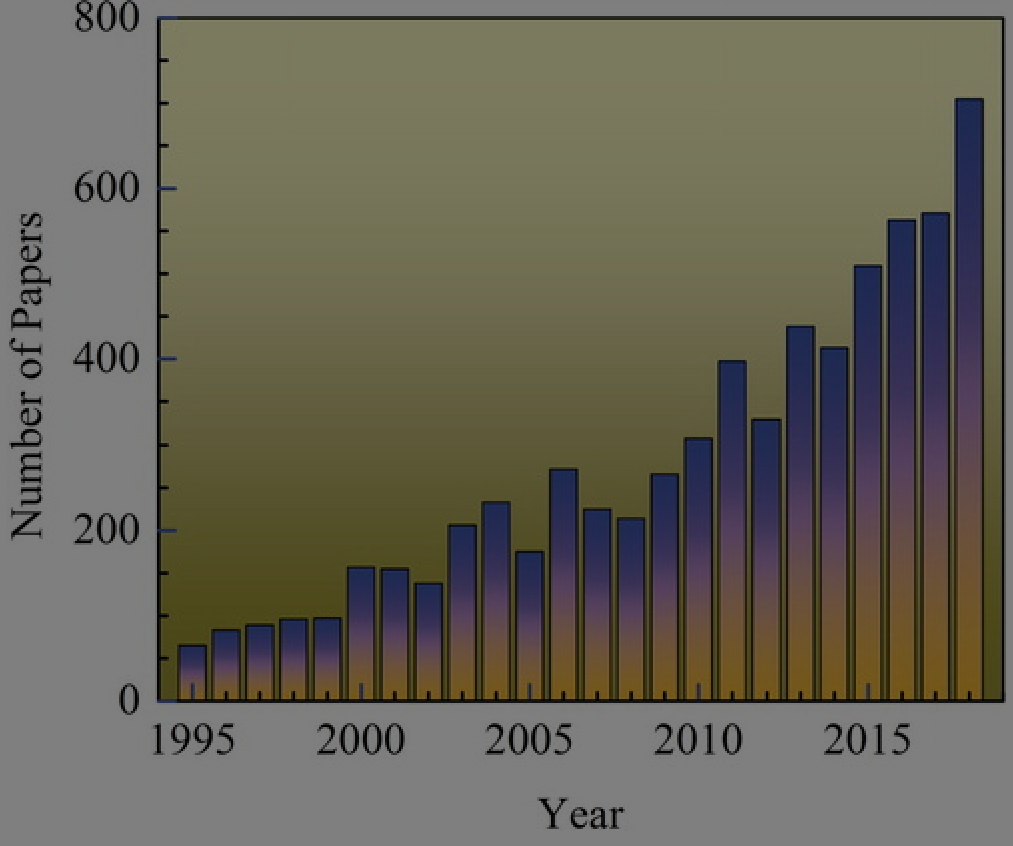

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HS materials have very diverse microstructures [1], including heterogeneous lamella structure [2], gradient structure [3–8], laminate structure [9,10], dual phase structure [11–13], harmonic structure [14–16], bi-modal structure [17–20], metal matrix composites [21–26], etc. These apparently very diverse structures have a common feature: all of them consist of both soft domains and hard domains with dramatically different flow stresses (or strength) [1].

During tensile deformation of HS materials, the soft domains will start plastic
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which in turn produces back-stress induced hardening, which helps with retaining ductility [1,2].

As described above, back stress is believed responsible for the strengthening and extra strain hardening observed in HS materials. Furthermore, various schemes to measure back stress from mechanical testing have been proposed [27,30,31], most equations for calculating back stress are based on concepts and assumptions instead of fundamental dislocation-based derivations. Back stress is also often associated with kinematic hardening, a term extensively used in the field of mechanics [32], which describes the mechanical phenomenon without addressing its physical origin. The concept and term of back stress are themselves still under debate in the materials community, with some researchers prefer to call them long-range internal stress [33,34]. Although back stress is usually small in homogeneous metals [27,35], it becomes significant for HS materials [1,2]. Therefore, it is of critical importance to understand the relationship between back stress and the mechanical behavior of HS materials.

In this perspective, we will briefly delineate the history of back stress, analyzing the development of back stress and forward stress in HS materials. We will show the inadequacy of using back stress to describe the strengthening and extra strain hardening in HS materials. In addition, back stress cannot be measured from mechanical testing, and the back-stress reported in the literature can be more accurately described as hetero-deformation induced (HDI) stress. We'll also briefly discuss the current fundamental issues that need to be investigated.

Brief h

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internal stress exerted on the matrix by precipitates. The internal stress proposed by Orowan and Fisher was later named back stress in a dislocation model by Ashby [43].

The back stress concept was later used by many groups to explain the strengthening of a metal matrix by second-phase particles in the 1970s [44–46]. More recently, back stress has been used to explain the hardening behavior and Bauschinger effect in TRIP steels [47], the transient plastic flow during creep [48], the Bauschinger effect in thin films [38], the hysteresis loop under cyclic loading [49], the extra strain hardening of HS materials [1,2,27,50,51], etc. These reports show that the back stress concept has been widely, if not fully, accepted by the materials community.

Dislocation models for back stress

Several dislocation models on the formation of back stress have been proposed [1,33,43,52–54]. The back stress is produced by geometrically necessary dislocations (GNDs). It is believed that GNDs are needed to accommodate the strain gradient in the gradient plasticity theory [28,29]. GNDs create lattice bending or misorientation, depending on their geometric pattern of arrangement. As shown in Figure 2, there are two basic types of GND arrangements. Figure 2(a) illustrates a pile-up of GNDs on a slip plane against a segment of the grain boundary, phase boundary, or domain boundary, which is hereafter referred to as the Type I GND arrangement. These GNDs have the same Burgers vector, and can be produced by dislocations emitted from a Frank-Read dislocation source. The GND pile-up produces a stress concentration of $n\tau_a$ at the
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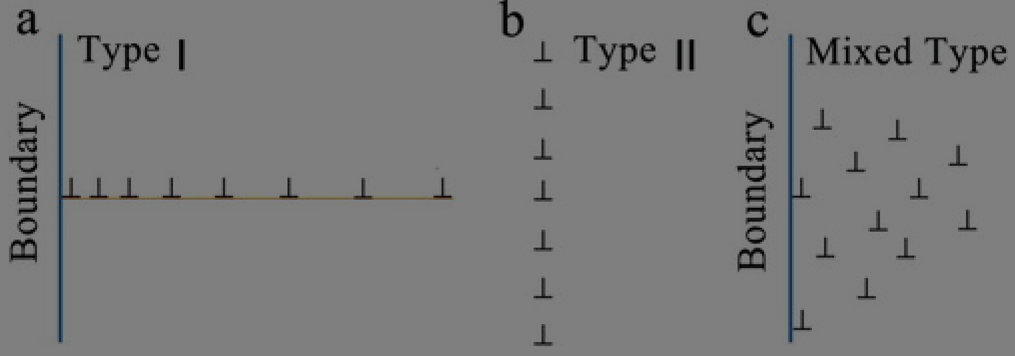

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Another basic type of GND arrangement is shown in Figure 2(b), which is essentially a tilt low-angle grain boundary. It is hereafter referred to as the Type II GND arrangement. It does not produce long-range internal stress, i.e. back stress [57]. However, internal stress exists in short range close to the tilt low-angle grain boundary. In a real situation such as bending of a crystal, a mixed type may exist [29], as shown in Figure 2(c), which does produce back stress but is not as effective as the Type I GND arrangement.

Back stress and mechanical properties

Back stress has been considered playing a critical role in the strengthening of metal matrix composites [44–46]. It is also often associated with Bauschinger effect [36,38,47,50]. However, neither back stress nor Bauschinger effect has been regarded as a major player in strengthening metallic materials by the general materials community. For example, in the literature and textbooks [58], listed mechanisms for strength
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is because the HS materials have great variation in flow stress from one domain volume to the next, which makes the back-stress induced strengthening and work hardening the primary players in the mechanical behavior. For example, an HS lamella Ti was found to have the strength of the ultrafine-grained Ti and uniform elongation higher than that of the coarse-grained Ti [2]. In addition, it also has strain hardening that is higher than the coarse-grained Ti. These mechanical behaviors cannot be explained by the conventional mechanisms in the textbooks. Therefore, back stress strengthening and work hardening have been used to explain the extraordinary mechanical properties of HS materials [1,2,27,60].

Issues with the back stress concept

As discussed above, back stress strengthening and work hardening have been believed responsible for the superior combination of strength and ductility of HS materials [1,2,39,61] as well as the Bauschinger effect [36,38,47,50]. With the fast development of the field of HS materials, it is of critical importance to clarify and understand how the back stress affects the mechanical behavior. Specifically, methods and equations have been proposed and developed to experimentally measure back stress from mechanical testing. Most of these methods and equations are not well anchored in deformation physics, i.e. dislocation mechanisms. A question arises on what is actually measured and if the measured 'back stress' is physically the global back stress in the materials.

To analyze this issue, let's look at the dislocation model of GND pile-up at an HS domain
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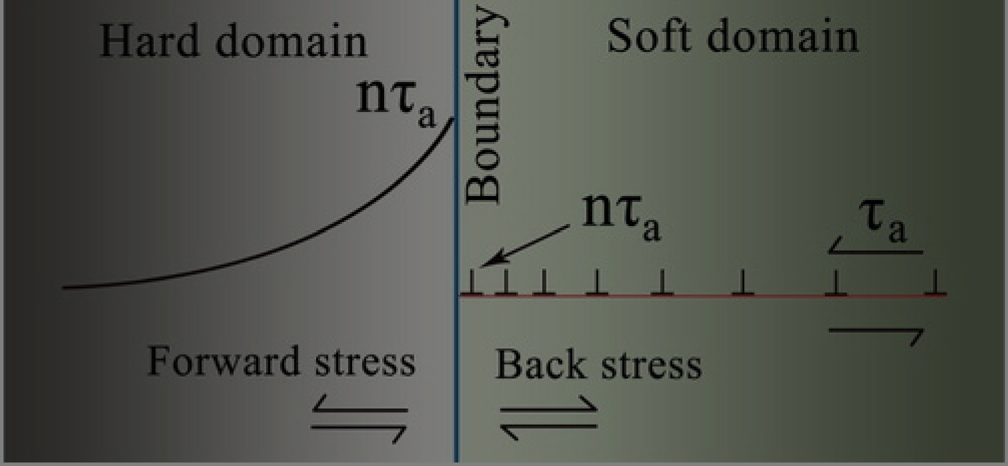

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Under the forward stress, the hard domain may behave in three different ways. Note that the forward stress in the hard domain near the domain boundary can be many times higher than the applied stress. First, if the hard domain is not much stronger than the soft domain, the leading dislocation at the head of a pile-up may be pushed into the domain boundary, which may lead to the emission of another dislocation from the boundary into the hard domain. In such a scenario, the buildup of back stress and forward stress is limited, and their influence on the mechanical behavior is also limited, as in the case of GND pile-ups at grain boundaries in conventional homogeneous materials. Second, if the hard domains are much stronger than the soft domains, the domain boundary will be much more effective in blocking GNDs, and the hard domain will remain elastic until the back stress is very high in the soft domain. This will increase the global yield stress and result in extra work hardening when both domains are deforming plastically, especially when the soft domain is fully constrained by the hard domain, as reported in the heterogeneous lamella Ti [2]. Third, if the hard domain is not

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suggests that it is logically not appropriate to attribute the unique mechanical behavior of HS materials to the back stress alone.

In the literature, back stress is measured by unloading-reloading curves in a tensile test [27], or from the unloading curves alone [30]. As shown in Figure 3, during unloading-reloading both the back stress and forward stress will be affected because they are coupled. Therefore, the unloading and reloading curves are affected by the interaction of the back stress and forward stress, instead of back stress alone. In other words, the back stress is not measurable from the mechanical testing curves, and the measured 'back stress' is not the real back stress in a physical sense. It should be noted that since the forward stress is induced by the back stress, we can logically regard the unique mechanical behavior of HS materials as induced by back stress. However, such a description can be misleading, since it may imply that the forward stress does not play a role.

New definition

As discussed above, a new term is needed to describe how the heterostructure affects the mechanical behavior and properties, because the current term, back stress, cannot represent the full physical process. At the fundamental level, the heterostructure leads to hetero-deformation among HS domains [1]. First, after the soft domains start yielding, the hard domains will remain elastic, which is a hetero-deformation scenario that produces back stress in the soft domain to raise the global yield strength. After the
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Outstanding issues

The definitions of HDI hardening and HDI stress raise some scientific issues for future study. First, the back stress and forward stress are coupled and act in opposite directions. It is not clear how they interact with each other to produce the HDI hardening and HDI stress. Recently, it has been observed that local shear bands are formed across domain boundaries [62]. This might be caused by local interactions between local back stresses and forward stresses. Second, the HDI stress (measured ‘back stress’ in the literature [2,27]) appears to increase quickly in the elastic-plastic deformation stage, but slows down during the plastic deformation stage, which need to be investigated. Third, GND pile-ups lead to the development of back stress, which in turn induces forward stress. It is also believed that GNDs are needed to accommodate strain gradient near domain boundaries. The relationships among back stress, forward stress, strain gradient and HDI stress need to be studied. Understanding these issues will help us with understanding the fundamental physics as well as the heterostructure-mechanical properties of HS materials.

Disclosure statement

No potential conflict of interest was reported by the authors.

Refer

1. Wu XL … unpre … doi: 10.

2. Wu XL … ltrafine-grain … 12:14501–14505

In this article

3. Lu K. Making strong nanomaterials ductile with gradients. Science. 2014;345:1455–1456. doi: 10.1126/science.1255940

| PubMed | Web of Science ® | Google Scholar

4. Wu XL, Jiang P, Chen L, et al. Extraordinary strain hardening by gradient structure. Proc Natl Acad Sci USA. 2014;111:7197–7201. doi: 10.1073/pnas.1324069111

| PubMed | Web of Science ® | Google Scholar

5. Wu XL, JIang P, Chen L, et al. Synergetic strengthening by gradient structure. Mater Res Lett. 2014;2:185–191. doi: 10.1080/21663831.2014.935821

| Web of Science ® | Google Scholar

6. Fang TH, Li WL, Tao NR, et al. Revealing extraordinary intrinsic tensile plasticity in gradient nano-grained copper. Science. 2011;331:1587–1590. doi: 10.1126/science.1200177

| PubMed | Web of Science ® | Google Scholar

7. Chen AY, Liu JB, Wang HT, et al. Gradient twinned 304 stainless steels for high strength and high ductility. Mater Sci Eng A. 2016;667:179–188. doi: 10.1016/j.msea.2016.04.070

| Web of Science ® | Google Scholar

8. Wei YJ, Li YQ, Zhu LC, et al. Evading the strength- ductility trade-off dilemma in steel

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9. Ma XL e laminates:

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0. Beyer nder

extren 0. doi:

10.10

In this article

1. Calcagnotto M, Adachi Y, Ponge D, et al. Deformation and fracture mechanisms in fine- and ultrafine-grained ferrite/martensite dual-phase steels and the effect of aging. Acta Mater. 2011;59:658–670. doi: 10.1016/j.actamat.2010.10.002

| Web of Science ® | Google Scholar

2. Li ZM, Pradeep KG, Deng Y, et al. Metastable high-entropy dual-phase alloys overcome the strength-ductility trade-off. Nature. 2016;534:227. doi: 10.1038/nature17981

| PubMed | Web of Science ® | Google Scholar

3. Park K, Nishiyama M, Nakada N, et al. Effect of the martensite distribution on the strain hardening and ductile fracture behaviors in dual-phase steel. Mater Sci Eng A. 2014;604:135–141. doi: 10.1016/j.msea.2014.02.058

| Web of Science ® | Google Scholar

4. Sawangrat C, Kato S, Orlov D, et al. Harmonic-structured copper: performance and proof of fabrication concept based on severe plastic deformation of powders. J Mater Sci. 2014;49:6579–6585. doi: 10.1007/s10853-014-8258-4

| Web of Science ® | Google Scholar

5. Zhang Z, Vajpai SK, Orlov D, et al. Improvement of mechanical properties in SUS304L steel through the control of bimodal microstructure characteristics. Mater Sci Eng A. 2014;598:106–113. doi: 10.1016/j.msea.2014.01.023

6. Vajpai ce Ti-6Al-4V alloy v ion. Metall Mater

7. Wang ured metal. Nature

×

In this article

8. Han BQ, Huang JY, Zhu YT, et al. Strain rate dependence of properties of cryomilled bimodal 5083 Al alloys. Acta Mater. 2006;54:3015–3024. doi: 10.1016/j.actamat.2006.02.045

Web of Science ® | Google Scholar

9. Han BQ, Lee Z, Witkin D, et al. Deformation behavior of bimodal nanostructured 5083 Al alloys. Metall Mater Trans A. 2005;36a:957–965. doi: 10.1007/s11661-005-0289-7

Web of Science ® | Google Scholar

0. Zhao YH, Topping T, Bingert JF, et al. High tensile ductility and strength in bulk nanostructured nickel. Adv Mater. 2008;20:3028–3033. doi: 10.1002/adma.200800214

Web of Science ® | Google Scholar

1. Liu J, Chen Z, Zhang FG, et al. Simultaneously increasing strength and ductility of nanoparticles reinforced Al composites via accumulative orthogonal extrusion process. Mater Res Lett. 2018;6:406–412. doi: 10.1080/21663831.2018.1471421

Web of Science ® | Google Scholar

2. Zhao L, Guo Q, Li Z, et al. Grain boundary-assisted deformation in graphene-Al nanolaminated composite micro-pillars. Mater Res Lett. 2018;6:41–48. doi: 10.1080/21663831.2017.1386241

Web of Science ® | Google Scholar

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25. Thilly L, Van Petegem S, Renault PO, et al. A new criterion for elasto-plastic transition in nanomaterials: application to size and composite effects on Cu-Nb nanocomposite wires. Acta Mater. 2009;57:3157–3169. doi: 10.1016/j.actamat.2009.03.021

Web of Science ® | Google Scholar

26. Tanaka K, Mori T. Hardening of crystals by non-deforming particles and fibres. Acta Metall. 1970;18:931. doi: 10.1016/0001-6160(70)90020-9

Google Scholar

27. Yang MX, Pan Y, Yuan FP, et al. Back stress strengthening and strain hardening in gradient structure. Mater Res Lett. 2016;4:145–151. doi: 10.1080/21663831.2016.1153004

Web of Science ® | Google Scholar

28. Gao HJ, Huang YG. Geometrically necessary dislocation and size-dependent plasticity. Scripta Mater. 2003;48:113–118. doi: 10.1016/S1359-6462(02)00329-9

Web of Science ® | Google Scholar

29. Ashby MF. Deformation of plastically non-homogeneous materials. Philos Mag. 1970;21:399. doi: 10.1080/14786437008238426

Web of Science ® | Google Scholar

30. Feaugas X. On the origin of the tensile flow stress in the stainless steel AISI 316 L at
300 K: doi:
10.10

31. Kuhlm tress and
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19

32. Bate F 34:1097–
1105.

In this article

3. Gibeling JC, Nix WD. A numerical study of long-range internal-stresses associated with subgrain boundaries. Acta Metall. 1980;28:1743–1752. doi: 10.1016/0001-6160(80)90027-9
Google Scholar

4. Levine LE, Geantil P, Larson BC, et al. Disordered long-range internal stresses in deformed copper and the mechanisms underlying plastic deformation. Acta Mater. 2011;59:5803–5811. doi: 10.1016/j.actamat.2011.05.056
Web of Science ® | Google Scholar

5. Phan TQ, Levine LE, Lee IF, et al. Synchrotron X-ray microbeam diffraction measurements of full elastic long range internal strain and stress tensors in commercial-purity aluminum processed by multiple passes of equal-channel angular pressing. Acta Mater. 2016;112:231–241. doi: 10.1016/j.actamat.2016.04.035
Web of Science ® | Google Scholar

6. Liu XL, Yuan FP, Zhu YT, et al. Extraordinary Bauschinger effect in gradient structured copper. Scr Mater. 2018;150:57–60. doi: 10.1016/j.scriptamat.2018.03.007
Web of Science ® | Google Scholar

7. Mompiou F, Caillard D, Legros M, et al. In situ TEM observations of reverse dislocation motion upon unloading in tensile-deformed UFG aluminium. Acta Mater. 2012;60:3402–3414. doi: 10.1016/j.actamat.2012.02.049

8. Xiang a Mater.
2006;

9. Tay c-6061
alumi /0921-
5093(

×

40. Bauschinger J. Über die Veränderung der Elasticitätsgrenze und der Festigkeit des Eisens und Stahls durch Strecken und Quetschen, durch Erwärmen und Abkühlen und durch oftmal wiederholte Beanspruchung. Mitteilungen aus dem mechanisch-technischen Laboratorium der k. polytechnischen Schule. München. 1886;13:1–115.
Google Scholar

41. Orowan E. Classification and nomenclature of internal stresses. J Inst Met. 1947;73:47–59.
Google Scholar

42. Fisher JC, Hart EW, Pry RH. The hardening of metal crystals by precipitate particles. Acta Metall. 1953;1:336–339. doi: 10.1016/0001-6160(53)90109-6
Google Scholar

43. Ashby MF. Work hardening of dispersion-hardened crystals. Philos Mag. 1966;14:1157–1178. doi: 10.1080/14786436608224282
Web of Science ® | Google Scholar

44. Tanaka K, Mori T. Hardening of crystals by non-deforming particles and fibres. Acta Metall. 1970;18:931. doi: 10.1016/0001-6160(70)90020-9
Google Scholar

45. Mori T, Tanaka K. Average stress in matrix and average elastic energy of materials
with m 01-
6160(

46. Brown ll.
19

47. Kato H auschinger
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10.23

8. Gan W, Zhang PH, Wagoner RH, et al. Effect of load redistribution in transient plastic flow. Metall Mater Trans A. 2006;37a:2097–2106. doi: 10.1007/BF02586130

| Web of Science ® | Google Scholar

9. Fournier B, Sauzay M, Caes C, et al. Analysis of the hysteresis loops of a martensitic steel - Part II: study of the influence of creep and stress relaxation holding times on cyclic behaviour. Mater Sci Eng A. 2006;437:197–211. doi: 10.1016/j.msea.2006.08.087

| Web of Science ® | Google Scholar

0. Hu XZ, Jin SB, Zhou H, et al. Bauschinger effect and back stress in gradient Cu-Ge alloy. Metall Mater Trans A. 2017;48a:3943–3950. doi: 10.1007/s11661-017-4176-9

| Web of Science ® | Google Scholar

1. Yuan FP, Yan DS, Sun JD, et al. Ductility by shear band delocalization in the nano-layer of gradient structure. Mater Res Lett. 2019;7:12–17. doi: 10.1080/21663831.2018.1546238

| Web of Science ® | Google Scholar

2. Mughrabi H. On the role of strain gradients and long-range internal stresses in the composite model of crystal plasticity. Mater Sci Eng A. 2001;317:171–180. doi: 10.1016/S0921-5093(01)01173-X

| Web of Science ® | Google Scholar

3. Mughr … w stress of
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4. Jen … e
Bausc … ter.
2012;

In this article

55. Hughes DA, Hansen N, Bammann DJ. Geometrically necessary boundaries, incidental dislocation boundaries and geometrically necessary dislocations. Scripta Mater. 2003;48:147–153. doi: 10.1016/S1359-6462(02)00358-5

| Web of Science ® | Google Scholar

56. Hull D, Bacon DJ. Introduction to dislocations. 3rd ed. Oxford: Pergamon Press; 1984.

Google Scholar

57. Hirth JP, Lothe J. Theory of dislocations. 2nd ed. Malabar (FL): Krieger Publishing Company; 1992.

Google Scholar

58. Hertzberg RW. Deformation and fracture mechanics of engineering materials. 3rd ed. New York: Wiley; 1989.

Google Scholar

59. Kassner ME, Geantil P, Levine LE. Long range internal stresses in single-phase crystalline materials. Intl J Plasticity. 2013;45:44–60. doi: 10.1016/j.ijplas.2012.10.003

| Web of Science ® | Google Scholar

60. Ma XL, Huang CX, Xu WZ, et al. Strain hardening and ductility in a coarse-grain/nanostructure laminate material. Scripta Mater. 2015;103:57–60. doi: 10.10

61. Xu R,

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10.

62. Huang ngth and

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